

1 **Prioritization of Rail Defect Inspection: A Risk-Based Optimization Approach**

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Kang Zhou

Ph.D. Student
Department of Civil and Environmental Engineering
Rutgers, The State University of New Jersey
96 Frelinghuysen Road, Piscataway, NJ 08854-8018
Tel: 732-319-5177; Email: kang.zhou@rutgers.edu

Xiang Liu, Ph.D., Corresponding Author

Assistant Professor
Department of Civil and Environmental Engineering
Rutgers, The State University of New Jersey
96 Frelinghuysen Road, Piscataway, NJ 08854-8018
Tel: 848-445-2868; Email: xiang.liu@rutgers.edu

Yu Zhou, Ph.D.

The Key Laboratory of Road and Traffic Engineering of the Ministry of Education
Tongji University, No.4800, Cao'an Road, Jiading district, Shanghai, China, 201804
Tel: +86-21-69589880; Email: yzhou2785@tongji.edu.cn

5740 Words + 1 Table and 6 Figures = 7490 words

August 1, 2016

1 ABSTRACT

2 Broken rail is the most common type of mainline derailment cause on freight railroads in the
3 United States. Detection and removal of rail defects is important for reducing the risk due to
4 broken-rail-caused derailments. The current practice is to periodically inspect rails using non-
5 destructive technologies, particularly ultrasonic inspection. Determining and prioritizing the
6 frequency of rail defect inspection is an important decision in broken rail risk management. This
7 paper develops a generalized, risk-based mixed integer nonlinear programming (MINLP) model
8 that can optimize segment-specific rail defect inspection frequency to minimize route broken rail
9 risk under limited inspection resources. A number of numerical examples are used to illustrate
10 the application of the model. This analysis shows that the use of an optimization approach can
11 result in a reduction of broken rail risk compared to an empirical heuristic that all segments on
12 the same route are inspected at an equal frequency. The optimization algorithm is being
13 implemented into a computer-aided decision support tool called “Rail Risk Optimizer” that can
14 automatically recommend an optimal segment-specific ultrasonic rail defect inspection
15 frequency given risk factors such as rail age and traffic density. The flexible research
16 methodology and the practice-ready optimization tool can potentially assist the railroad industry
17 to mitigate broken rail risk in a cost-efficient manner.

18
19 *Keywords:* Broken rail, Ultrasonic inspection, Risk optimization, Decision support tool

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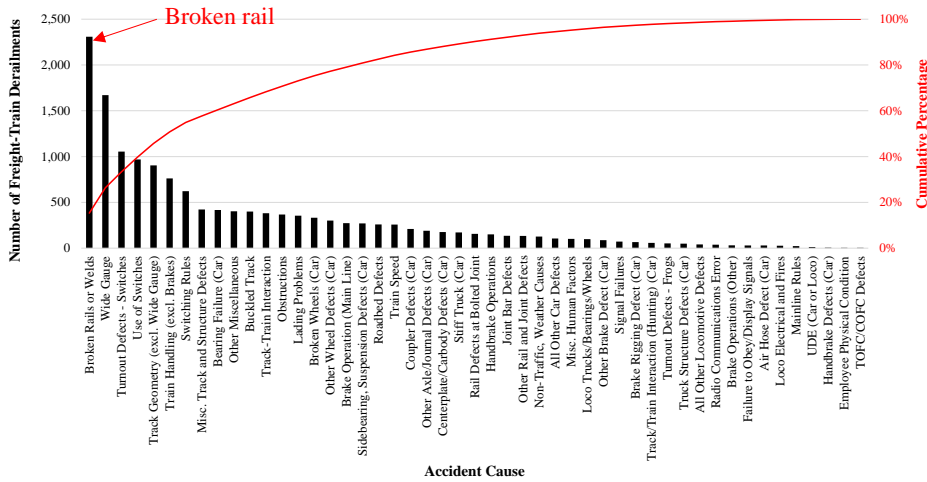
1 1 INTRODUCTION

2 Railway transportation is vital for the U.S. economy. While society derives significant benefits
3 from rail transportation, there are attendant risks that must be managed and reduced. Train
4 accidents cause damage to infrastructure and rolling stock, disrupt services, and may cause
5 casualties and harm the environment (1-3). Although the U.S. freight-train accident rate has
6 declined by over 80 percent since 1980 (2), accidents still present a major safety concern. For
7 instance, all types of train accidents resulted in about 360 million dollars' worth of reported
8 damage costs and ~~878853~~ casualties in 2015, [in which approximately 500 casualties were caused
9 by train derailments or collisions and about 320 casualties were caused by high-rail accidents](#)(4).

10 Derailment is the most common type of freight-train accident on mainlines in the U.S.,
11 accounting for approximately 72% of all types of accidents (1). In light of continual growth in
12 nationwide rail traffic, a further reduction in derailment risk is a high priority for both the
13 railroad industry and the Federal Railroad Administration (FRA) (5). A train derailment can be
14 due to different accident causes. The FRA categorizes over 400 accident causes into five major
15 groups: track, equipment, human factors, signal, and miscellaneous. Each of these broad
16 groupings contains respective subgroups with a number of detailed causes. It is important to note
17 that different accident causes have different accident frequencies (6). Among all freight-train
18 derailment causes, broken rails or welds are the most frequent (Figure 1a), making broken rail
19 prevention and risk management a high-profile activity in the U.S. rail industry.
20 Transverse/compound fissures, detail fractures and vertical split head are the three main types of
21 rail breaks among all types of rail defects classified by the FRA (Figure 1b). These three defects
22 are caused by the fatigue growth of internal rail defects due to cyclic loading by passage of trains
23 (7). There are various approaches to preventing broken rails, including rail grinding (8),
24 lubrication (9), rail replacement (10), and nondestructive rail defect inspection (11-13). This
25 paper focuses on ultrasonic rail defect inspection, a primary rail defect detection technology used
26 by American railroads since 1930s (14). Ultrasonic rail defect inspection can provide a non-
27 destructive detection of internal rail defects. The detection information can be used for
28 maintenance and operational actions to prevent a potential derailment.

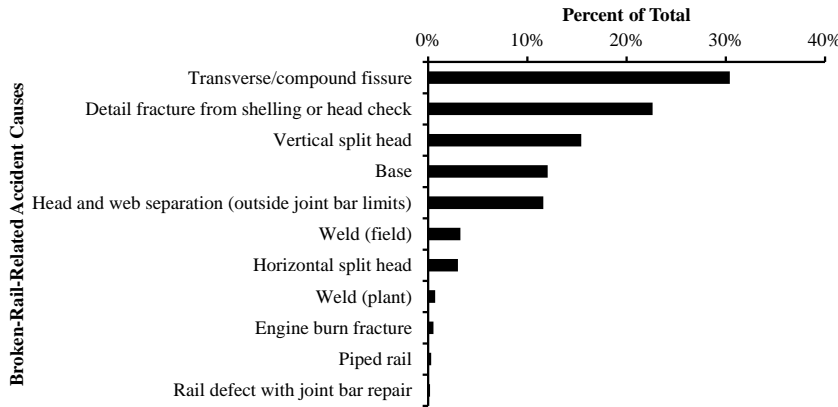
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FIGURE 1(a) Frequency of accident cause, Class I mainline freight train derailments, all types of tracks, 2001 to 2014



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FIGURE 1(b) Distribution of Class I railroad mainline freight train derailments by broken-rail-related accident causes, 2001 to 2014

10 Understanding the relationship between the occurrence of broken rails and the inspection
 11 frequency can aid the rail industry to prioritize and allocate cost-effective inspection resources.
 12 Previous studies have found that different track segments can have different broken rail risks.
 13 Increasing inspection frequencies on certain high-risk segments can significantly reduce the total
 14 risk (15-17). This finding indicates that the prioritization of rail defect inspection may minimize
 15 the total risk given equal or even fewer mileages inspected. The current practice is to inspect all
 16 the segments of the same route with an equal annual frequency. An alternative strategy might be

1 to inspect more frequently the segments that have higher risks. As we will discuss in later
2 sections, this alternative approach requires more sophisticated risk modeling and optimization
3 techniques.

4 The objective of this paper is to develop a generalized methodological framework that
5 can optimize segment-specific rail defect inspection frequency given total miles of track to
6 inspect. This model uses input information such as traffic density and rail age to estimate
7 segment-specific broken rail risk, and use the risk information to optimize the frequency of
8 ultrasonic rail testing. This paper is structured as follows. First, we review the relevant literature,
9 identify knowledge gaps and elaborate on the scope of this research. Second, we present a
10 generalized risk-based optimization methodology to determine the optimal rail defect inspection
11 scheduling by segment characteristics. Third, we illustrate the application of the model using
12 scenario-based numerical analyses and draw new managerial insights on broken rail risk
13 management. Finally, we summarize principal research findings and suggest possible future
14 research directions.

15 **2 LITERATURE REVIEW AND OBJECTIVES OF THIS STUDY**

16 **2.1 Literature Review**

17 This section reviews relevant studies in the areas of the occurrence of broken rails, broken rail
18 statistical prediction, and inspection frequency scheduling.

19 1) *Occurrence of broken rails.* Several types of defects might occur to the rail, such as
20 longitudinal defects, transverse defects, base defects, and others (18). Transverse defects related
21 to metal fatigue are one of the most common severe defects leading to rail service failures and
22 train derailments (15, 19). Studies have found that rail design, rolling stock characteristics,
23 inspection, and maintenance schedules all affect broken rail risk. The mechanism of rail crack
24 formation and growth through theoretical modeling and laboratory testing has been extensively
25 studied in the literature (11, 20-23).

26 2) *Broken rail statistical prediction.* In addition to engineering analysis, the prior effort also
27 predicted broken rail occurrence using statistical approaches. For example, Shry and Ben-Akiva
28 (24) developed a survival function and a hazard function to predict the rail condition. Dick (25)
29 evaluated the factors affecting broken rail service failures and derailments using a multivariate
30 analysis of predictor variables. Dick et al. (26) further developed a broken rail prediction model
31 to estimate broken rail risk given rail age, rail weight and several other factors. Sourget and
32 Riollot (27) developed two models for prediction of broken rails: logistic regression and decision
33 trees. A general model to estimate the total number of broken rail between two successive rail
34 defect inspections is developed by the Volpe National Transportation Systems Center (8, 11, 12).
35 Using the outputs of the Volpe model, Liu et al. (15) developed an exponential model to
36 correlate broken rail rate with inspection frequency, and found that the higher the inspection
37 frequency, the lower the broken rail risk, given all else being equal. In the United Kingdom,
38 Zhao et al. (16, 17) also found that an exponential function can approximately describe the
39 relationship between annual number of broken rails per track-mile and inspection frequency.

40 3) *Inspection frequency scheduling.* Liu et al. (28) developed an optimal condition-based
41 rail inspection frequency that incorporates the effect of the seasonal variation. Liu et al. (15)
42 proposed an analytical model to optimize the inspection interval based on the risk category (low
43 risk, medium risk, and high risk). Following the inspection, Orringer et al. (29) studied a delayed
44 action concept for prioritizing immediate repair of critical defects (those with a large defect size),
45 while delaying repair of non-critical defects within a defined grace period.
46

1

2 **2.2 Knowledge Gaps**

3 While the knowledge of broken rail risk management continues to grow, there are several areas
4 for further research. On the subject of rail defect inspection, the prior research either assumed
5 that all segments are inspected at an equal frequency (empirical heuristic) (12, 30) or the
6 segments whose broken rail risks are within the same risk category are inspected at an equal
7 frequency (group-based inspection strategy) (7, 31). To our knowledge, there is no published
8 study that explicitly models segment-specific inspection frequency. All the existing and
9 emerging inspection schedules are within these scenarios. Given a large number of possible
10 inspection schedules, which one would lead to the lowest number of broken rails under resource
11 constraints? For instance, instead of inspecting all segments at four times per year, can we
12 prioritize more inspections on certain segments that can minimize the route risk, without
13 requiring additional miles of inspection? This research is developed to address these questions.

14

15 **2.3 Research Objectives and Scope**

16 To ensure a deep understanding of rail inspection issues within the content limit, this research
17 focuses its effort on fatigue-related rail defects, including detail fractures, transverse defects, and
18 vertical split head defects. Other types of rail defects or track geometry defects are beyond the
19 scope of this paper, but shall be addressed in a separate detailed study. Also, this paper focuses
20 on defective rails for freight railroads, without considering passenger or transit rails. This
21 research aims to address the following objectives:

- 22 • Develop a generalized risk-based optimization methodology that can prioritize the
23 allocation of inspection resources to different track segments with heterogeneous risks.
- 24 • Implement the methodology into a computer-aided decision support tool for
25 automatically computing location-specific broken rail risk and recommending optimal
26 inspection schedules.
- 27 • Provide new insights regarding the effects of traffic density, rail age, and other factors on
28 rail inspection scheduling.

29

30 **3 METHODOLOGY**

31 The risk-based rail defect inspection frequency optimization methodology comprises of two
32 modules, 1) the estimation of broken rails by inspection frequency and 2) the prioritization of
33 segment-specific inspection frequency given the total miles to inspect.

34

35 **3.1 Estimation of Number of Broken Rails by Inspection Frequency**

36 A number of factors can affect the rate of broken rails, such as temperature differential, rail age,
37 traffic density, curvature, roadbed condition, axle load, vehicle dynamics, rail wear, and others
38 (24-27). The Volpe National Transportation Systems Center has developed an engineering model
39 that incorporates rail defect formation, growth, and detection processes (11, 12). According to
40 the Volpe model, a rail defect is assumed to form at an increasing rate as the rail ages due to the
41 accumulation of tonnage. The model for the rate of defect formation is derived based on a
42 Weibull distribution. The Weibull distribution model was calibrated based on observations of
43 defect occurrence at the Facility for Accelerated Service Testing (FAST) at the Transportation
44 Test Center in Pueblo, Colorado and on several segments of revenue track studied by the
45 Association of American Railroads. After a defect was formed, its size progression was
46 calibrated from the original detail fracture growth test conducted at FAST and has been further

1 verified and validated by tests conducted through a joint international research effort supported
 2 by the Union of International Railways/World Executive Council (32, 33). Temperature
 3 differential, axle load, track modulus, rail wear, and other factors were found to affect defect size
 4 growth. The probability of detecting a rail defect depends on the [defect location, defect size,](#)
 5 [equipment inspection technology used and etc-and-the-size-of-the-defect](#). Although larger defects
 6 are more likely to be detected, they still can be missed during the inspection process (34). The
 7 Volpe model focuses on rail fatigue defects, such as detail fractures, transverse/compound
 8 fissures, and vertical split head defects. Note that the Volpe model was developed in 1990s based
 9 on the rail infrastructure conditions during that time period. We are unaware of recent updates to
 10 this model. This may introduce some level of uncertainty when applying this model to predict
 11 rail defects under today's infrastructure conditions. A more detailed description of the Volpe
 12 model has been provided in Orringer (12), and thus not duplicated herein.

13
 14 The Volpe model is presented as follows.

$$16 \quad y_{(i-1,i)} = R \times \frac{e^{-\frac{N_{i-1}}{\beta} y^\alpha} - e^{-\frac{N_{i-1} + X_i}{\beta} y^\alpha}}{1 + \lambda(X_i - \mu)} \times \lambda(X_i - \mu) \quad (1)$$

17 Where:

18 $y_{(i-1,i)}$ = number of broken rails per track-mile between the (i-1)th and ith inspection

19 R = 39-foot rail segments per track-mile, 273

20 X_i = interval (million gross tons (MGT)) between the (i-1)th and ith inspection

21 α = Weibull shape factor, 3.1 (35)

22 β = Weibull scale factor, 2150 (35)

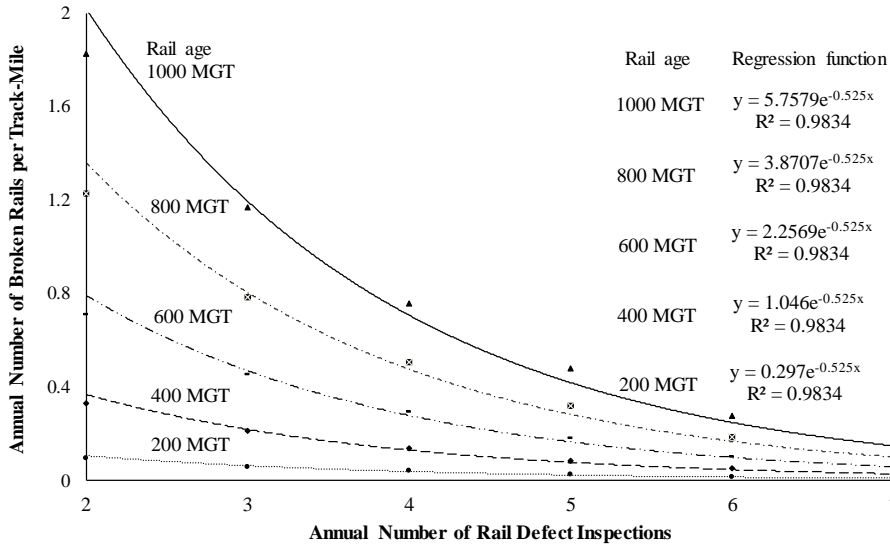
23 λ = slope of the number of rail breaks per detected rail defect (S/D) versus inspection interval
 24 curve, 0.014 (12)

25 μ = minimum rail inspection interval, 10 MGT (12)

26 N_i = rail age (cumulative tonnage on the rail) at the ith inspection, $N_i = N_{i-1} + X_i$

27
 28 The parameters in Equation (1) are based on published statistics in the literature. As
 29 stated earlier, broken rail occurrence is subject to many engineering factors. In the absence of
 30 detailed information for all these factors, this paper uses the two focused factors, rail age and
 31 traffic density, in the Volpe model. The methodology can be adapted to other factors or an
 32 updated version of the Volpe model in future research. Figure 2 calculates annual number of
 33 broken rails per track-mile given different rail ages (when traffic density is 80 MGT per year)
 34 using the Volpe model. Each data point represents the estimated number of broken rails given the
 35 number of ultrasonic rail defect inspections per year using Equation (1). Through a nonlinear
 36 regression, the number of broken rails per track-mile can be estimated by an exponential function
 37 of annual inspection frequencies. For example, at 1000 MGT rail age and 80 MGT annual traffic
 38 density, the relationship between the annual number of broken rails and inspection frequency is
 39 fitted as an exponential function $y=5.7579 \exp(-0.525x)$, where y is the annual number of broken
 40 rails per track-mile, and x is the annual inspection frequency. The coefficient of determination R^2
 41 is more than 0.98, indicating a reasonable goodness of fit. If a track segment of this is inspected
 42 four times annually ($x=4$), the approximate number of broken rails per track-mile is
 43 $0.7579 \times \exp(-0.525 \times 4)=0.093$. If this segment is 10-miles long, the annual broken rail

1 frequency on this segment would be $0.093 \times 10 = 0.93$. The analysis also shows that given the
 2 same inspection frequency, the higher the rail age, the higher the broken rail risk.
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 6 **FIGURE 2 Relationship between number of broken rails and annual rail defect inspection**
 7 **frequency (assuming that annual traffic density is 80 MGT)**
 8

9 Similarly, an exponential regression model is found to adequately fit the data given other
 10 rail ages and traffic densities. A general exponential model is presented as follows:

11
 12
$$y = a \times \exp(bx) \tag{2}$$

13 where:

- 14 y = the total number of broken rails per track-mile per year;
- 15 x = annual rail inspection frequency on the track segment;
- 16 a and b are the model parameters which are dependent on the rail age and annual traffic density,
- 17 and other factors. These model parameters can be obtained through the regression method.

18
 19 **3.2 Rail Inspection Frequency Optimization**

20 Suppose that there are n track segments on the whole rail track with different rail ages and
 21 annual traffic densities. The available inspection resource is B . In this paper, the inspection
 22 resource is specified in terms of the total miles inspected. Each track segment may have its own
 23 inspection frequency (denoted as x_i). The theoretical premise is that inspecting high-risk track
 24 segments more frequently may lead to a minimization of total route risk, with the equal or even
 25 fewer miles inspected. This premise was shown to be valid in Liu and Dick (31) who classify
 26 hazardous materials transportation risks into three categories (low, medium and high), and
 27 required all segments within each category to have the same inspection frequency. This paper

1 significantly advances the study by Liu and Dick (31) by relaxing the requirement for group-
 2 specific inspection scheduling to segment-specific inspection scheduling. In essence, the work
 3 developed in Liu and Dick (31) is viewed as a special and simplified case of the generalized
 4 methodology developed here.

5 Because there are numerous possible inspection schedules to choose from, the
 6 enumeration approach is computationally cumbersome in identifying the optimal solution.
 7 Therefore, this research uses a mathematical optimization technique, which is devised to achieve
 8 a predetermined objective under constraints. In the context of rail inspection frequency, a
 9 generalized model is presented below:

$$11 \text{ MINIMIZE } \sum_{i \in N} y_i \times l_i \quad (3)$$

12 where

$$13 y_i = a_i \times e^{b_i x_i}$$

14 Subject to

$$16 \sum_{i \in N} x_i \times l_i \leq B \quad (4)$$

$$17 x_i \geq 0 \quad (5)$$

18 where

19 y_i = total number of broken rails per track mile per year

20 x_i = annual rail inspection frequency

21 l_i = the mileage of segment i ;

22 other parameters are previously defined.

23
 24 The objective function is to minimize the total number of broken rails on the whole route
 25 given the total miles inspected. The first constraint (Equation 4) imposes the inspection resource
 26 availability restriction. The second constraint (Equation 5) specifies the non-negative integer
 27 decision variables. The model parameters a_i and b_i can be determined based on the rail age and
 28 annual traffic density of each segment. Given the total miles inspected per year, the optimization
 29 model can be used to determine the minimum number of broken rails with an optimal allocation
 30 scheduling of inspection frequencies to each segment.

31 The optimization model represents a mixed integer nonlinear programming problem
 32 (MINLP). As one of the most challenging optimization models, the computational complexity of
 33 this problem increases dramatically when the number of track segments increases. For example,
 34 consider a route comprising ~~of~~ 100 segments. Each segment can be inspected at a frequency
 35 ranging from 2 to 7 inspections per year. Therefore, there are a total of 6^{100} (about 3700 trillion)
 36 possible scenarios of rail inspection schedules for this route. Therefore, the enumeration method
 37 or most of the off-the-shelf software cannot solve such a complex model. In an extensive review
 38 of the operations research literature, the authors find that an advanced algorithm called the Outer
 39 Approximation (OA) (36-40) is particularly useful for solving this type of complex optimization
 40 problem. The mathematical details of the OA algorithm can be found in (37).

41 3.3 Decision Support Tool

42 A computer-aided decision support tool is developed at Rutgers University to implement the
 43 complex model formulation and solution algorithms into a practice-ready tool that can
 44

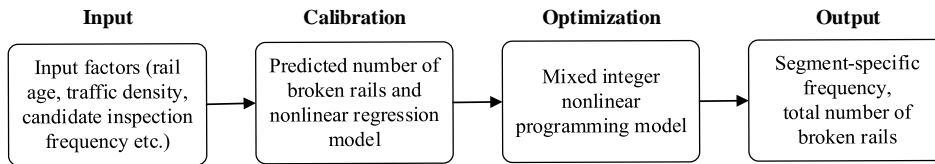
1 automatically generate various rail defect inspection schedules, estimate their corresponding
 2 broken rail risks, and identify optimal scheduling, given any level of resource availability. The
 3 decision support tool contains four major modules as illustrated in Figure 3.

4 *Input Module:* The user provides track-segment information such as rail age and annual
 5 traffic density. Also, the user specifies the maximum resources available (i.e. total miles
 6 inspected) and other constraints.

7 *Calibration Module:* Based on segment-specific information, the calculation module
 8 firstly estimate the total number of broken rails per track-mile given the annual inspection
 9 frequency on each segment, using the Volpe model presented earlier. Based on the Volpe model
 10 output, a nonlinear regression model will be developed to approximate the number of broken
 11 rails by annual inspection frequency.

12 *Optimization Module:* After an exponential regression function is calibrated to describe
 13 the relationship between the total number of broken rail per track-mile and the annual inspection
 14 frequency, a mixed integer nonlinear programming model is developed to determine segment-
 15 specific inspection frequency. The objective is to minimize the total number of broken rails
 16 given total miles of inspection.

17 *Output Module:* The outputs include the minimum route risk that can be achieved by
 18 using the optimal inspection scheduling, and the corresponding segment-specific inspection
 19 frequency are recommended.



20
 21 **FIGURE 3 Schematic of decision support tool for optimizing segment-specific inspection**
 22 **frequency**
 23

24
 25 **4 NUMERICAL EXAMPLE**

26 To illustrate the model application, several hypothetical scenarios are performed for a tangent
 27 track with 10 track segments. All segments are assumed to have an equal length of 7.2 miles. The
 28 scenarios encompass different rail ages that would affect broken rail risk. Through these scenario
 29 analyses, this study analyzes the impact of different factors on rail inspection frequency
 30 optimization.

31
 32 **4.1 Optimal Inspection Frequency under Resource Constraint**

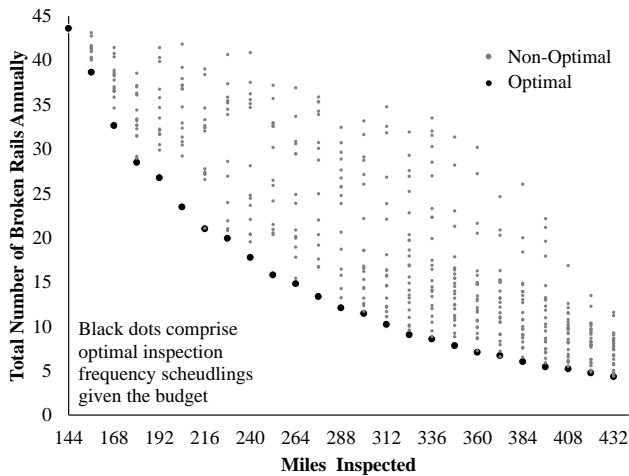
33 Suppose that the whole track has the uniform annual traffic density of 80 MGT. Segment-
 34 specific rail ages are as follows. For illustration, we assume heterogeneous segment rail ages.
 35 The methodology is applicable to other rail age distributions.

36

Segment ID	A	B	C	D	E	F	G	H	I	J
Rail Age (MGT)	400	700	500	400	600	400	500	900	300	200

37
 38 Each track segment can have an annual inspection frequency of 2, 3, 4, 5, 6, or 7. In total,
 39 there are 6^{10} (600 million) possible combinations of rail inspection frequency schedules on this

1 route. The numbers of broken rails for possible rail inspection schedules were estimated and
 2 plotted. With the same number of miles to be inspected for each inspection schedule, some
 3 inspection schedules resulted in lower broken-rail risk than others. The inspection schedules
 4 resulting in the lowest level of the number of broken rail given a total mileage to inspect were
 5 denoted as the “optimal” schedules. Other alternative inspection schedules were called “non-
 6 optimal” schedules. These “optimal” schedules constitute a Pareto frontier (Figure 4). The Pareto
 7 frontier demonstrates the optimal inspection scheduling given limited inspection resources. For
 8 example, given a total of 288 miles inspected, the optimal inspection frequency for each segment
 9 on this route is (3, 6, 4, 4, 5, 4, 4, 6, 2, 2), with the minimal total annual number broken rails on
 10 this route as 12. One of alternative inspection schedules denoted by gray dots is (4, 6, 5, 2, 3, 3, 3,
 11 5, 5, 4), with the total number of broken rails as 15. Therefore, the “optimal” schedule may
 12 reduce broken rail risk than its alternatives given the same inspection resources.
 13



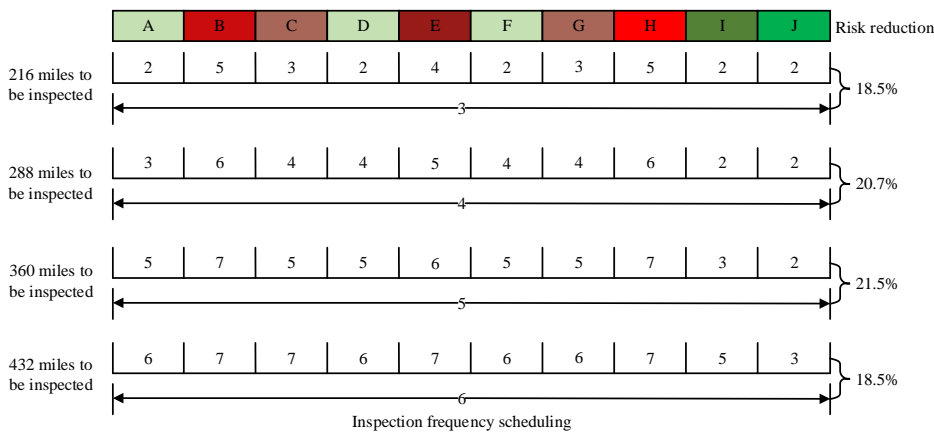
14 **FIGURE 4 Illustration of Pareto optimization of rail defect inspection frequency given total**
 15 **miles to inspect**
 16

17
 18 The analysis shows that given total miles inspected, there exists an optimal inspection
 19 frequency schedule that can lead to a minimum broken rail risk. On the Pareto-frontier, the more
 20 miles to inspect, the lower broken rail risk under the optimal schedule. The Pareto-frontier may
 21 vary with track and traffic factors (e.g., rail age, traffic density, segment mileage), the next
 22 subsection will perform a scenario analysis to better understand how the optimal inspection
 23 frequency by segment may change with these factors.
 24

25 **4.2 Comparison between Optimization-based Scheduling versus Empirical Approach**

26 In this section, we analyze the amount of broken rail risk reduction using the optimization-based
 27 rail defect inspection schedule versus the empirical approach that all the segments of the same
 28 route are inspected at equal frequencies. We consider four total miles for inspection 216, 288,
 29 360, 432, respectively. For example, “216” means that the railroad has resources to inspect a
 30 total of 216 miles per year on this route. We compare two inspection frequency scheduling

1 approaches. The first approach is an empirical approach that all the segments are inspected at an
 2 equal frequency. This approach is treated as a baseline in the analysis and the predicted number
 3 of broken rails is called “base risk”. An alternative approach is to optimize segment-specific
 4 inspection frequency using the MINLP model described in this paper. Railroads often use a
 5 road–rail vehicle (aka. hi-rail vehicle) that can operate both on railway tracks and on
 6 conventional roadways to inspect rail defects. This type of inspection method allows for different
 7 inspection frequencies on different track segments. Skipping the inspection of certain lower-risk
 8 segments might enable more frequent inspections of higher-risk track segments, thus maximizing
 9 the risk reduction. The minimum number of broken rails optimized by this model is regarded as
 10 “optimization risk”. Figure 5 illustrates the inspection frequency scheduling for each track
 11 segment and the risk reduction of broken rail risk between the two approaches.
 12
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 16 **FIGURE 5 Schematic illustration of ultrasonic rail inspection frequency**
 17 **on each track-segment**
 18

19 Remark:
$$\text{Risk reduction} = \frac{(\text{Base risk} - \text{Optimization risk})}{\text{Base risk}} \times 100\%$$

20
 21 For example, given 216 inspection mileages, if an empirical schedule calls for all track
 22 segments to be inspected three times per year; this schedule could be denoted as (3, 3, 3, 3, 3, 3,
 23 3, 3, 3, 3). An alternative risk-based optimal inspection schedule could be (2, 5, 3, 2, 4, 2, 3, 5, 2,
 24 2). Compared with the empirical schedule (with an inspection of all track segments three times
 25 per year), the optimal inspection schedule would reduce the broken rail number by 18.5%. With
 26 216 inspection miles per year, the annual inspection frequency for segment B and H increase to 5
 27 from the average inspection frequency 3, while the annual inspection frequency for segment A,
 28 D, F, I and J decreases to 2 (Figure 5). This is not surprising because segment B and H have
 29 higher rail ages than other segments. As shown in Figure 2, a higher rail age is associated with a
 30 higher broken rail risk, given all else being equal.
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**TABLE 1 Optimal Inspection Schedules for Different Time Periods
(Assuming the Annual Traffic Density 80 MGT)**

Optimal Inspection Frequency by Segment (<i>Italic Numbers</i>)												
Time Period	Segment	A	B	C	D	E	F	G	H	I	J	Risk reduction compared to the equal-frequency approach
In three years	Rail Age											
	Miles Inspected	640	940	740	640	840	640	740	1140	540	440	
	216	<i>3</i>	<i>4</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>4</i>	<i>2</i>	<i>2</i>	8.5%
	288	<i>4</i>	<i>5</i>	<i>4</i>	<i>4</i>	<i>5</i>	<i>4</i>	<i>4</i>	<i>5</i>	<i>3</i>	<i>2</i>	9.3%
	360	<i>5</i>	<i>6</i>	<i>5</i>	<i>5</i>	<i>6</i>	<i>5</i>	<i>5</i>	<i>6</i>	<i>4</i>	<i>3</i>	9.3%
432	<i>6</i>	<i>7</i>	<i>6</i>	<i>6</i>	<i>7</i>	<i>6</i>	<i>6</i>	<i>7</i>	<i>5</i>	<i>4</i>	9.3%	
In five years	Rail Age											
	Miles Inspected	800	1100	900	800	1000	800	900	1300	700	600	
	216	<i>3</i>	<i>4</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>4</i>	<i>2</i>	<i>2</i>	5.5%
	288	<i>4</i>	<i>5</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>5</i>	<i>3</i>	<i>3</i>	5.5%
	360	<i>5</i>	<i>6</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>6</i>	<i>4</i>	<i>4</i>	5.5%
432	<i>6</i>	<i>7</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>7</i>	<i>5</i>	<i>5</i>	5.5%	
In seven years	Rail Age											
	Miles Inspected	960	1260	1060	960	1160	960	1060	1460	860	760	
	216	<i>4</i>	<i>4</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>4</i>	<i>2</i>	<i>2</i>	3.2%
	288	<i>4</i>	<i>5</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>5</i>	<i>3</i>	<i>3</i>	3.2%
	360	<i>5</i>	<i>6</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>6</i>	<i>4</i>	<i>4</i>	3.2%
432	<i>6</i>	<i>7</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>7</i>	<i>5</i>	<i>5</i>	3.2%	
In ten years	Rail Age											
	Miles Inspected	1200	1500	1300	1200	1400	1200	1300	1700	1100	1000	
	216	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>3</i>	<i>4</i>	<i>3</i>	<i>2</i>	0.7%
	288	<i>4</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>4</i>	<i>5</i>	<i>4</i>	<i>3</i>	0.7%
	360	<i>5</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>5</i>	<i>6</i>	<i>5</i>	<i>4</i>	0.7%
432	<i>6</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>6</i>	<i>7</i>	<i>6</i>	<i>5</i>	0.7%	

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In the empirical schedule, the inspected miles allocated on the segments with rail age 500 MGT or more account for 50 percent of the total amount of inspection resources. However, for the optimal schedule, this percentage has increased to 67 percent. It indicates that more frequent inspection of higher-risk track segments (higher rail ages in this example) would further reduce broken rail risk.

4.3 Comparison of Current Inspection Frequency Versus in the Future

As the traffic on each track segment accumulates, the rail age for each track segment should increase. For example, if the initial rail age for one segment is 400 MGT, and the annual traffic density is 80 MGT. In five years, the rail age for the segment will increase to $400+80 \times 5=800$ MGT if there is no replacement of the rail. Table 1 shows the estimated rail age for each track segment in different time periods and illustrates the optimal inspection schedules for each track-segment given various total miles inspected in three years, five years, seven years and ten years.

Based on Table 1, we find that segment-specific optimal inspection schedules would change as the rail age for each track segment increases. For example, given a total of 288 track miles of inspection on the route per year, segment B currently has an optimal schedule of six (6) inspections per year. In three years, five years and seven years from now, its optimal schedule would be five (5) times per year. In ten years, its inspection frequency becomes 4, given the same total route mileage for inspection (Figure 6a). While the optimal inspection frequency for segment B decreases in future, more inspections will be allocated to other segments (e.g., segment I). This is probably because the relative differences of risk levels between different segments reduce if their rail ages become relatively closer to each other, given all else being equal. For example, at present, segment B's rail age is 700 MGT, while segment C's rail age is 500 MGT (29% difference). In ten years (annual traffic density of 80 MGT within the period), this relative difference of rail age reduces to 13%. A similar phenomenon was also found when the total inspection resources change (Figure 6b). To summarize, if the relative differences of broken risks among track segments reduce, the optimal schedule is similar to the empirical approach that most of the segments on the same route are inspected with the equal frequency. Note that the risk can be affected by rail age and other factors. This paper focuses on the effect of rail age. The methodology can be adapted to other factors in future research.

	A	B	C	D	E	F	G	H	I	J	Risk reduction
At present	3	6	4	4	5	4	4	6	2	2	20.7%
In three years	4	5	4	4	5	4	4	5	3	2	9.3%
In five years	4	5	4	4	4	4	4	5	3	3	5.5%
In seven years	4	5	4	4	4	4	4	5	3	3	3.2%
In ten years	4	4	4	4	4	4	4	5	4	3	0.7%

FIGURE 6(a) Schematic illustration of ultrasonic rail inspection frequency on each track-segment for each time period (given 288 miles to be inspected)

	A	B	C	D	E	F	G	H	I	J	Risk reduction
At present	6	7	7	6	7	6	6	7	5	3	18.5%
In three years	6	7	6	6	7	6	6	7	5	4	9.3%
In five years	6	7	6	6	6	6	6	7	5	5	5.5%
In seven years	6	7	6	6	6	6	6	7	5	5	3.2%
In ten years	6	6	6	6	6	6	6	7	6	5	0.7%

FIGURE 6(b) Schematic illustration of ultrasonic rail inspection frequency on each track-segment for each time period (given 432 miles to be inspected)

5 RESEARCH CONTRIBUTION

- This research develops a new risk-based methodology to optimize the inspection frequency for each segment, with the goal of minimizing the risk with equal or fewer inspection resources. The scenario simulation results show that effective scheduling of rail defect inspections could reduce the risk of broken rails in a cost-efficient manner.
- Using the methodology developed, a decision support tool entitled the “Rail-Risk Optimizer” is produced. This decision support tool can practically be used to prioritize resource allocation while improving the safety effectiveness of ultrasonic rail defect inspections at the same time. This would be done through determining more efficient inspection schedules in which higher-risk segments might be inspected more frequently than lower-risk segments.

6 CONCLUSION

This research develops a risk-based methodology to optimize the inspection schedules for each track segment given a certain amount of inspection resources available. The methodology was used in scenario simulations to demonstrate the safety effectiveness of optimizing rail inspection frequency schedules. The analysis showed that prioritizing more inspections on certain higher-risk segments will minimize the total route risk with minimal additional inspection resources. Also, rail age was found to be an important influencing factor. If the percentage differences of rail ages among track segments of the same route are small, inspecting all segments with equal frequencies will lead to a near-optimum inspection schedule. If this is not the case, there could be a further reduction in broken rail risk if the optimization approach is used. The research here holistically provides a generalized methodology to quantify segment-specific broken rail risk in an effort to aid decision makers in arranging their most proper rail defect inspection schedules.

7 LIMITATIONS OF CURRENT RESEARCH & FUTURE RESEARCH

This paper focused on how to determine segment-specific inspection frequency under a certain amount of inspection resources, thus minimizing broken rail risk. The current practice allows for adjacent segments to be inspected with different frequencies. If the inspection vehicles (hi-rail vehicles) get on and off the track too frequently, it will cause practical inconvenience. In future research, a “stretch constraint” should be added into the optimization model in order impose a

1 restriction on the minimum mileage within which the inspection frequency is homogenous. In
 2 addition, this paper adopts the Volpe model developed in 1990s, which had no update for more
 3 than 25 years. It might bring about some uncertainty for predicting rail defects. In the future, an
 4 update for the Volpe mode is needed based on more recent rail defect data. Furthermore, future
 5 research can adapt this methodology to account for other types of rail defects. Lastly, to better
 6 understand the sensitivity of optimal inspection scheduling to a variety of track characteristics
 7 (segment length, traffic density and so on), more analyses involving varying scenarios will be
 8 developed in future research.

10 ACKNOWLEDGEMENT

11 The first author was funded by the Department of Civil and Environmental Engineering (CEE)
 12 through a research fellowship at Rutgers University. The authors thank Daniel Rodriguez for his
 13 assistance. However, the authors are solely responsible for all views and analyses in this paper.

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